

OPTICAL DIGITAL-TO-ANALOG CONVERTER

Government Contact

The Government has a paid-up license in this invention and the right in limited
5 circumstances to require the patent owner to license others on reasonable terms as
provided for by the terms of Contract No. MDA972-03-C-0046 awarded by DARPA.

Related Applications

United States Patent application Application Serial No. 10/133,469 was filed
on April 26, 2002, and United States Patent application Application Serial No.
10 10/674,722 was filed on September 3, 2003.

Technical Field

This invention relates to optical waveform generation systems and, more
particularly, to conversion of digital signals into analog optical signals.

Background of the Invention

15 Digital-to-analog (D/A) converters are key elements in both electronic and
photonic signal processing and data transmission. In many optical transmission
systems, digital data has to be converted to analog form for processing and/or
transmission. Indeed, there are many advantages for using optical technology to
implementing D/A converters, for example, high-speed clocking and signal sampling,
20 wide-bandwidth, light-weight components and the like. Additionally, a high-speed
arbitrary analog waveform generator can be implemented using a very high-speed
D/A converter.

One such optical D/A converter is described in an article entitle "Digital-to-
Analog Conversion Using Electrooptic Modulators", authored by A. Yacoubian et al.,
25 IEEE Photonics Technology Letters, Vol. 15, No. 1, January 2003, pages 117-119.
However, the disclosed implementation is limited to a so-called 2-bit photonic D/A
converter.

Summary of the Invention

These and other problems and limitations of prior known optical modulation
30 arrangements are overcome in applicants' unique invention by utilizing a continuous
wave or pulsed laser optical signal, which is split into a plurality of mutually coherent
optical beams. Each of the plurality of optical beams is phase shift modulated by bits

(control signals) of a data sequence to generate a corresponding plurality of phase shift modulated mutually coherent optical signals. The modulated optical signals are recombined to form the desired digital-to-analog converted optical signal for use as desired.

5 In one specific embodiment of the invention, the phase modulation is effected by splitting optical signal comprising a continuous wave laser optical signal into a plurality of similar mutually coherent optical signals, phase shift modulating the continuous wave optical coherent signal of each of the similar continuous wave laser optical signals with the digital data bits (control signals). Then, the plurality of phase
10 shifted modulated continuous wave optical signals are combined to yield the resulting converted digital-to-analog signal.

In another embodiment of the invention, the supplied digital data sequence is preprocessed via a processor before the data bits of the sequence are supplied to modulate the plurality of mutually coherent versions of the supplied continuous wave
15 laser optical signal.

In yet another embodiment of the invention, a pulsed laser signal is supplied as an input to the optical digital-to-analog converter. The pulsed laser optical signal is split into a plurality of mutually coherent optical beams, which are phase shift modulated by data sequences stored in a memory to generate a substantially jitter free
20 analog optical signal after the phase shift modulated optical beams are recombined. The pulsed laser optical signal is controlled to have the same repetition rate as the data sequence from the memory unit. By properly aligning the data sequence with the pulses of the pulsed laser optical signal, the effect of timing jitter is canceled.

In still another embodiment of the invention, instead of stacking more phase
25 shift modulators in a single stage digital-to-analog converter, a plurality of digital-to analog converter stages having fewer phase shift modulators are cascaded to form the over all digital-to-analog converter, in accordance with the invention. This embodiment of the invention is advantageous to realize a desired distribution of discrete output levels.

30 **Brief Description of the Drawing**

FIG. 1 shows, in simplified block diagram form, one embodiment of the invention;

FIG. 2 also shows, in simplified block diagram form, a second embodiment of the invention;

5 FIG. 3 illustrates, in simplified block diagram form, a third embodiment of the invention; and

FIG. 4 shows, in simplified block diagram form, details of a fourth embodiment of the invention.

10

Detailed Description of Embodiments of the Invention

FIG. 1 shows, in simplified block diagram form, one embodiment of the invention. Specifically, shown is optical light source 101 typically including a continuous wave or pulsed laser to generate an optical signal at a desired wavelength. Exemplary optical signals to be processed have optical frequencies of about 2.3×10^{14} Hertz to about 1.8×10^{14} Hertz, i.e., a wavelength of about 1.3 microns to about 1.7 microns. In one example, a continuous wave optical signal having a wavelength of approximately 1.55 microns, i.e., a frequency of 1.93×10^{14} Hertz, is generated by light source 101 and supplied via 102 to optical digital-to-analog converter 100. In optical digital-to-analog converter 100 the continuous wave optical signal is supplied via optical path 103 to splitter 104, which generates a plurality of N mutually coherent optical beams 105-1 through 105-N. The number N of the mutually coherent beams has to be at least two (2), but four (4) to eight (8) optical beams are typically employed. The importance of the plurality N of optical beams being mutually coherent in this application will be discussed below. In this example, splitter 104 is a multimode interference (MMI) coupler. The plurality N of mutually coherent optical beams are supplied on a one-to-one basis to a corresponding plurality of optical phase shifters 106-1 through 106-N, respectively. Also supplied via 112-1 through 112-N to phase shifters 106-1 through 106-N are bits, i.e., control signals, of a data sequence for causing the phase shifts in phase shifters 106-1 through 106-N to effect the desired digital-to-analog conversion. Thus, in this example, the digital-to-analog conversion is

realized by use of an electro-optical phase shift modulation scheme through either direct phase shift modulation of the continuous wave optical beams from laser 101 or by an external phase shift modulation using, for example, a Mach Zehnder phase shift modulator. The frequency of the modulation signal is in the microwave/millimeter-wave range. The phase shift modulated outputs from phase shifters 106-1 through 106-N are supplied via optical paths 107-1 through 107-N, respectively, to optical combiner 108, where they are recombined to form the desired optical analog signal. In this example, combiner 108 is a multimode interference (MMI) coupler. This analog optical signal is supplied via optical paths 109 and 110 to linear photodiode 111, which yields an electrical signal for use as desired.

The recombined phase shift modulated optical signal being detected by photodiode 111 develops current i_{PD} through photodiode 111 which is calculated as follows:

$$i_{PD} = RP_m \left| \sum_i \exp\left(j\pi \frac{V_i}{V_\pi}\right) \right|^2,$$

where R is the responsivity of photodiode 111, P_{in} the launched optical power, V_i the control voltage for the i -th phase shift modulator and V_π the switching voltage for a phase shift modulator. If the control voltages are now configured such that each of them can have two different levels, namely, $V_{i,low}$ and $V_{i,hi}$, 2^i output current i_{PD} levels are realizable. If the two different control voltage levels $V_{i,low}$ and $V_{i,hi}$ are switched between at a “high” rate an arbitrary waveform is developed at the output of photodiode 111. The so-called “high” rate is typically 10-40 Gbits/s, but could be as high as 160 Gbits/s.

The phase shift modulator 106 of each branch can be fabricated e.g. in a material system with linear electro-optic effect, as InP, GaAs or LiNbO₃. The effective refractive index of an optical waveguide changes in proportion to the applied electrical field perpendicular to this waveguide. A high frequency distributed electrical waveguide is engineered to co-propagate with the optical wave with matched propagating velocity to deliver the local electrical field with high modulation

bandwidth. The different branches will delay the optical signal by a different length of time. This results in different phases at the outputs of phase shifters 106. In the combiner 108, these different output phase signals that interfere constructively have a different optical signal phase due to the different time delays these signals experienced. The resulting optical signal after the MMI coupler, i.e., combiner 108, is the sum of all the phase shifted optical signals that interfere constructively.

FIG. 2 also shows, in simplified block diagram form, a second embodiment of the invention. The embodiment of FIG. 2 is similar to that of FIG. 1 and includes similar elements that are essentially identical from both a physical and functional standpoint. These similar elements have been similarly numbered as those in FIG. 1 and will not be discussed again in detail. The only significant difference between the embodiments of FIG. 1 and FIG. 2 is the use of processor 201. As can be seen, one or more data signals are supplied to processor 201 via input connection 202. In processor 201, the data signals are employed to code and generate control voltage signals for driving, phase shift modulators 106-1 through 106-N. These control voltage signals are supplied via output connections 112-1 through 107-N to phase shifters 106-1 through 106-N, respectively.

FIG. 3 illustrates, in simplified block diagram form, a third embodiment of the invention. The embodiment of FIG. 3 is also similar to that of FIG. 1 and includes similar elements that are essentially identical from both a physical and functional standpoint. These similar elements have been similarly numbered as those in FIG. 1 and will not be discussed again in detail. The only significant difference between the embodiments of FIG. 1 and FIG. 3 is that a pulsed laser signal is supplied as an input from pulsed laser 301 to the optical digital-to-analog converter 100, and that the pulsed laser optical signal 102 is controlled to have the same repetition rate as the data sequence from memory unit 302. The pulsed laser optical signal is split into a plurality of mutually coherent optical beams 105-1 through 105-N via splitter 104, which are phase shift modulated via phase shifters 106-1 through 106-N by data sequences stored in a memory to generate a substantially jitter free analog optical signal after the phase shift modulated optical beams are recombined. The pulsed laser

optical signal 102 is controlled via clock 303 to have the same repetition rate as the data sequence from memory unit 302. By properly aligning the data sequence with the pulses of the pulsed laser optical signal, the effect of timing jitter is canceled.

5 FIG. 4 shows, in simplified block diagram form, details of another digital-to-analog converter 100 in accordance with the invention. In this embodiment a plurality of digital-to-analog converter stages 100-1 through 100-J are cascaded in order to realize a desired number of phase shift modulated optical beams in obtaining the overall digital-to-analog conversion. As noted above at least two (2) branches are
10 required in each stage with an overall number of stages being two (2) to four (4), i.e., between four (4) and eight (8) branches of optical beams to be phase shift modulated by the bits of the data sequence, i.e., the control voltage signals. This analog optical signal is supplied via optical paths 109 and 110 to linear photodiode 111, which yields an electrical signal for use as desired. This embodiment is advantageous to realize a
15 desired distribution of discrete output levels.

The recombined phase shift modulated optical signal being detected by photodiode 111 develops current i_{PD} through photodiode 111, which is calculated as follows:

$$i_{PD} = RP_m \prod_j \left| \sum_i \exp\left(j\pi \frac{V_{i,j}}{V_\pi}\right) \right|^2,$$

20 where j is the running index for the j -th stage.

The above-described embodiments are, of course, merely illustrative of the principles of the invention. Indeed, numerous other methods or apparatus may be devised by those skilled in the art without departing from the spirit and scope of the
25 invention.